Bubble and Dew Point Measurements of the Ternary System Carbon Dioxide + Methanol + Hydrogen at 313.2 K

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Gas-expanded liquids offer many advantages as superior solvents for asymmetric hydrogenation reactions. To implement such applications, knowledge of the phase behavior of hydrogen with these tunable solvents is imperative. Phase boundary data are reported for the ternary system of carbon dioxide, methanol, and hydrogen at 313.2 K and pressures up to 21.7 MPa. The data were measured in a variable-volume windowed vessel by visual observation of one- to two-phase transitions.

Introduction

Gas-expanded liquids (GXLs) are highly tunable mixtures of organic solvents with a gas, where both the solvent power and the transport properties change significantly with concentration (pressure). CO_2 is generally the gas used because high concentrations require only modest pressures and it is inexpensive, nontoxic, and nonflammable. GXLs offer advantages for reactions¹⁻⁴ and separations.⁵⁻⁷ Compared to regular solvents, GXLs afford increased solubility of gases, enhanced mass transfer, a measure of tunability of solvent strength, and the additional safety provided by a nonflammable solvent. Compared to supercritical or liquid CO₂, GXLs afford higher solubility of reactants and catalysts at significantly lower pressures. GXLs are especially attractive for homogeneously catalyzed multiphase reactions between reactants in the gas phase and those in the liquid phase because gases tend to have higher solubilities than liquids. Such reactions might include hydrogenation with H₂, oxidation with O₂, and hydroformylation with CO. Because many of these reactions are carried out under pressure anyway, the capital investment for the highpressure equipment related to CO_2 is less of an issue.

Many properties of CO2-expanded liquids have been reported, such as viscosity,^{8,9} diffusion coefficients,^{8,10,11} solubility,^{12,13} and solvatochromic shift.^{14,15} For ternary systems of GXLs that include two gaseous species, some critical and phase boundary data¹⁶⁻¹⁹ are available. Although abundant vapor-liquid equilibrium data are available for the CO_2 + methanol, H_2 + methanol, and H_2 + CO_2 binary systems,²⁰ there are few phase equilibrium data available for the ternary system of CO_2 + methanol + H_2 . Previous measurements at (278, 288, and 298) K have been reported by Bezanehtak et al.²¹ Because hydrogenation reactions are being carried out in CO₂-expanded methanol in our laboratories and others,^{1,22} we report the phase boundaries of the ternary system containing hydrogen, carbon dioxide, and methanol at 313.2 K measured synthetically in a variable-volume windowed vessel.

Experimental Section

Chemicals. Methanol (Aldrich, 99.93% HPLC grade, anhydrous) was used as received. Carbon dioxide (Mathe-





Figure 1. Variable-volume windowed pressure vessel.

son, SFC grade) and hydrogen (Air Products, ultrahigh purity) were passed through gas purifiers.

Apparatus. Phase transitions were observed in a McHugh-type variable-volume windowed pressure vessel (Figure 1) reported previously.^{23,24} The working volume of the pressure vessel could be varied from 5 mL to 20 mL with a piston, moved by an aqueous dye solution on the backside, connected to a syringe pump (ISCO model 260 D). The blue color of the aqueous dye solution is easily detectable through the window of the vessel should the O-ring on the piston fail. The entire cell was placed in a thermostated air bath (modified Varian 3400 gas chromatograph) with temperature control better than ± 0.2 °C. The temperature was measured with a handheld readout (HH-22 Omega) and thermocouple (Omega Type K) inserted into the center of the phase equilibrium vessel. The thermocouple response time was on the order of seconds. The combination of thermocouple and readout was accurate to ± 0.2 °C and calibrated for each experiment against a platinum RTD (Omega PRP-4) with a DP251 Precision RTD benchtop thermometer (DP251 Omega) accurate to ± 0.025 °C and traceable to NIST. Back pressure was applied to the piston with a syringe pump (ISCO 100D) operated at constant pressure.

Methanol was introduced into the windowed pressure vessel with a six-port valve and injection loops (Valco) of known calibrated volumes. Another syringe pump (ISCO model 260 D) filled with compressed CO_2 was connected to one port of the six-port valve to meter CO_2 into the vessel. Methanol was injected through the injection loop with a gastight syringe (VWR) while the CO_2 flowed directly through to the vessel. As the valve was switched to position 2, the sample contained in the loop was displaced by CO_2 and carried into the vessel.

The temperatures in the windowed pressure vessel, the transfer vessel for H_2 (discussed below), and the syringe

pump for CO_2 were measured to ± 0.1 °C with type K thermocouples (Omega), which were previously calibrated in a hot point cell (Omega) and connected to digital temperature indicators (HH-22 Omega). The pressures in the windowed pressure vessel, the transfer vessel for H₂, and the syringe pump for CO_2 were measured to ± 0.07 bar with pressure transducers (Druck Limited, DPI 260 read-out PDCR-3040 transducer), which were calibrated against a hydraulic dead weight tester (Ruska). The vessel contents were mixed with a magnetic stir bar coupled with an external magnet. The phase behavior in the vessel was observed through the sapphire window with a borescope camera (Olympus F100-024-000-55), placed through the wall of the GC oven.

Procedure. The oven was controlled to 40 $^{\circ}$ C, and the backside volume was filled with the aqueous dye solution, taking care to avoid air bubbles. The vessel was mounted on the rack inside the GC oven and then connected to a syringe pump used to control pressure and to monitor volume changes.

Before each experiment, the air from the system was purged by pressurizing the system to 10 bar with CO_2 and then depressurizing, twice repeated. When the CO_2 purging process was completed, the piston in the variable-volume vessel was at its full range of travel. The volume reading on the controller of the backside syringe pump was recorded, and from the change of this volume reading, the volume of the $H_2 + CO_2 + MeOH$ ternary system in the vessel was calculated.

The vessel was filled with a known volume of methanol through the six-port valve with an injection loop of known volume; the uncertainty of added methanol is ± 0.001 mol or, for the smallest loading, an error of $\pm 2\%$ in moles added. The injection loop was first filled with anhydrous methanol using a gastight syringe, and the methanol was carried into the vessel by CO₂ when the valve was switched. CO₂ and H₂ were subsequently added to the vessel.

 $\rm CO_2$ was loaded from the syringe pump set to a constant volumetric flow rate between 0.01 and 1.00 mL/min. Before loading, the volume and pressure readings on the pump controller and the temperature reading on the digital temperature indicator were recorded. During and after the loading, the temperature of $\rm CO_2$ in the pump may change. After the temperature was stable, the volume, temperature, and pressure readings were recorded. The $\rm CO_2$ density at specified temperature and pressure was calculated with the Span–Wagner equation of state.²⁵ The amount of $\rm CO_2$ added to the vessel was calculated from the volume readings and the $\rm CO_2$ densities before and after loading with an uncertainty of ± 0.001 mol or, for the smallest loading, an error of $\pm 1.5\%$ in moles added.

 $\rm H_2$ was introduced into the vessel from a transfer vessel of known volume and temperature by pressure difference. Before and after loading, the stable temperatures and the pressures of the H_2 transfer vessel were recorded. The H_2 density at the specified temperature and pressure was calculated from the truncated virial expression and second virial coefficient from DIPPR²⁶ with an uncertainty of ± 0.0015 mol or, for the smallest loading, an error of $\pm 20\%$ in moles added.

Visual observation of phase separation was used to measure the phase boundary of the H_2 - CO_2 -MeOH ternary system. In a typical run, the volume of the H_2 + CO_2 + MeOH ternary system was decreased by increasing the pressure until the H_2 + CO_2 + MeOH ternary system made the transition from two phases to one homogeneous phase. During this process, the liquid level increased until



Figure 2. Bubble point data for the CO_2 + methanol binary system at 313.2 K: \bigcirc , Ohgaki and Katayama;²⁷ \blacktriangle , this work.

Table 1. Bubble Point Data for the $CO_2(1)$ + Methanol (2) Binary System at 313.2 K

phase boundary pressure <i>P</i> /bar	CO_2 mole fraction x_1
9.3	0.051
35.7	0.205
48.5	0.291
63.1	0.411
74.9	0.591
76.8	0.653
79.3	0.786

there was only one transparent liquid phase. After the temperature in the vessel was stable, the volume of the H₂-CO₂-MeOH ternary system was increased slowly by decreasing the pressure slightly until the cloud point was observed where the emergence of uniform bubbles in the liquid scatter light and cause a "black out" on the monitor. The last pressure when the liquid phase was still transparent was recorded, and the $H_2 + CO_2 + MeOH$ ternary system was pressurized back to this pressure. Smaller steps were used for further depressurization, and the pressurizing-depressurizing process was repeated at least three times for accuracy. The pressure and temperature in the vessel and the volume reading on the controller of the syringe pump for the aqueous dye solution were recorded. The process was repeated at least three times to verify the repeatability of the data point, and the average value was taken with the standard deviation for all points less than 0.4 bar. Additional H₂ or CO₂ was then added to the vessel for another measurement. When the pressure in the vessel exceeded 250 bar with the piston at the maximum volume position, the vessel was depressurized and cleaned to prepare for another series of experiments.

Results and Discussion

 CO_2 + *Methanol System.* The bubble points for the binary CO_2 + methanol system measured at 313.2 K are listed in Table 1. These data are in good agreement with those reported by Ohgaki and Katayama²⁷ as shown in Figure 2.

 $CO_2 + Methanol + H_2$ System. Phase boundary data for the ternary CO_2 + methanol + H₂ system obtained at 313.2 K are listed in Table 2. The solubility of H₂ in methanol + CO_2 mixtures, as shown in Figure 3, is linear with pressure, and the slope decreases with increasing CO_2 concentration. We were surprised that Henry's law was obeyed to concentrations as high as 0.2 mol fraction of H₂.



Figure 3. Hydrogen mole fraction in CO₂ (1) + methanol (2) at 313.2 K as a function of pressure and solute-free composition: \Box , $x_1 = 0$, Brunner et al.;³² \blacklozenge , $x_1 = 0.415$; \blacktriangle , $x_1 = 0.776$; \blacklozenge , $x_1 = 0.902$, this work.

Table 2. Phase Boundary Data for the $CO_2\ (1)$ + Hydrogen (2) + Methanol (3) Ternary System at 313.2 K

phase boundary pressure <i>P</i> /bar	CO_2 mole fraction x_1	${ m H}_2$ mole fraction x_2	$\begin{array}{c} {\rm MeOH\ mole} \\ {\rm fraction\ } x_3 \end{array}$	x_1/x_3	x_2/x_3	
87.9	0.410	0.011	0.579	0.71		BP
101.5	0.408	0.018	0.574	0.71		BP
129.6	0.402	0.032	0.566	0.71		BP
98.0	0.754	0.019	0.217	3.47		BP
124.0	0.735	0.053	0.212	3.47		BP
158.8	0.715	0.079	0.206	3.47		BP
190.3	0.696	0.103	0.201	3.47		BP
217.6	0.677	0.129	0.195	3.47		BP
99.2	0.872	0.032	0.095	9.17		BP
117.3	0.849	0.059	0.093	9.17		BP
138.4	0.827	0.083	0.090	9.17		BP
156.4	0.807	0.105	0.088	9.17		BP
166.2	0.787	0.127	0.086	9.17		BP
182.8	0.768	0.149	0.084	9.17		BP
187.1	0.746	0.172	0.081	9.17		BP
200.7	0.725	0.196	0.079	9.17		BP
199.7	0.699	0.236	0.064		3.67	DP
171.8	0.742	0.203	0.055		3.67	DP
146.5	0.777	0.176	0.048		3.67	DP
129.3	0.807	0.152	0.041		3.67	DP
120.0	0.824	0.139	0.038		3.67	DP

We attempted to predict the Henry's law constants from the correlation of previously measured binary vapor-liquid equilibria using the Peng-Robsinon equation of state. The α value for methanol was changed to that recommended by Stryjek and Vera.²⁸ The methanol + CO₂ vapor-liquid equilibria, which is a severe test of thermodynamic models,²⁹ was not satisfactorily correlated using the quadratic mixing rules; therefore, we examined the Huron-Vidal mixing rule³⁰ with the NRTL model ³¹ as our expression for $G^{\rm E}$ at infinite pressure. Our initial regression of the three binary pairs of interaction parameters gave a poor prediction of our experimental Henry's constants. We found that the methanol + H₂ interaction parameters were quite correlated. This is expected because we were regressing two parameters and the experimental range of our independent variable, H₂ mole fraction, varied only between 0 and 0.04. Using both the ternary and binary data, we were able to fit acceptable parameters for methanol + H₂, although as seen in Figure 4 the model does not give as sharp a drop in the Henry's constant as measured.

Conclusions

For the ternary $CO_2 + H_2$ + methanol system 313.2 K, the two-phase envelope contracts with increasing pressure.



Figure 4. Henry's constant of hydrogen in the CO_2 -expanded methanol mixture at 313.2 K. The curve is a prediction of Peng-Robinson with Huron-Vidal mixing rules.

The solubility of H_2 can be increased in the liquid phase with the addition of CO_2 to give a higher concentrations of H_2 at the same total pressure.

Literature Cited

- Combes, G. B.; Dehghani, F.; Lucien, F. P.; Dillow, A. K.; Foster, N. R. Asymmetric Catalytic Hydrogenation in CO₂ Expanded Methanol-aN Application of Gas Anti-Solvent Reactions (GASR). In *Reaction Engineering for Pollution Prevention*; Abraham, M. A., Hesketh, R. P., Eds.; Elsevier Science: Amsterdam, 2000; pp 173-181.
- (2) Musie, G.; Wei, M.; Subramaniam, B.; Busch, D. H. Catalytic Oxidations in Carbon Dioixde-Based Reaction Media, Including Novel CO₂-Expanded Phases. *Coord. Chem. Rev.* **2001**, 219–221, 789–820.
- (3) Subramaniam, B.; Lyon, C. J.; Arunajatesan, V. Environmentally Benign Multiphase Catalysis with Dense Phase Carbon Dioxide *Appl. Catal.*, B 2002, 37, 279–292.
 (4) Huang, Y.; Schricker, S. R.; Culbertson, B. M.; Olesik, S. V.
- (4) Huang, Y.; Schricker, S. R.; Culbertson, B. M.; Olesik, S. V. Synthesis of Poly(acrylic acid-co-itaconic acid) in Carbon Dioxide-Methanol Mixtures. J. Macromol. Sci., Pure Appl. Chem. 2002, A39, 27-38.
- (5) Eckert, C. A.; Bush, D.; Brown, J. S.; Liotta, C. L. Tuning Solvents for Sustainable Technology. Ind. Eng. Chem. Res. 2000, 39, 4615– 4621.
- (6) Zhao, J.; Olesik, S. V. Separation of Dimer Acids Using Enhanced-Fluidity Liquid Chromatograpy. Anal. Chim. Acta 2001, 449, 221–236.
- (7) Lin, C.; Muhrer, G.; Mazzotti, M.; Subramaniam, B. Vapor-Liquid Mass Transfer during Gas Antisolvent Recrystallization: Modeling and Experiments. *Ind. Eng. Chem. Res.* 2003, 42, 2171– 2182.
- (8) Frank, M. J. W.; Kuipers, J. A. M.; van Swaaij, W. P. M. Diffusion Coefficients and Viscosities of $CO_2 + H_2O$, $CO_2 + CH_3OH$, $NH_3 + H_2O$, and $NH_3 + CH_3OH$ Liquid Mixtures. J. Chem. Eng. Data **1996**, 41, 297–302.
- (9) Kho, Y. W.; Conrad, D. C.; Knutson, B. L. Phase Equilibria and Thermophysical Properties of Carbon Dioxide-Expanded Fluorinated Solvents. *Fluid Phase Equilib.* 2003, 206, 179–193.
- (10) Funazukuri, T.; Ishiwata, Y. Diffusion Coefficients of Linoleic Acid Methyl Ester, Vitamin K₃, and Indole in Mixtures of Carbon Dioxide and *n*-Hexane at 313.2 K, and 16.0 MPa. and 25.0 MPa. *Fluid Phase Equilib.* **1999**, *164*, 117–129.
- (11) Mantell, C.; Rodriguez, M.; Martinez de la Ossa, E. Measurement of the Diffusion Coefficient of a Model Food Dye (malvidin 3,5diglucoside) in a High-Pressure CO₂ + Methanol System by the Chromatographic Peak-Broadening Technique. J. Supercrit. Fluids 2003, 25, 57-68.
- (12) Liu, Z.; Li, D.; Yang, G.; Han, B. Solubility of Organic Acids in Ethyl Acetate Expanded with CO₂. *Fluid Phase Equilib.* 2000, 167, 123–130.
- (13) Wei, M.; Musie, G. T.; Busch, D. H.; Subramaniam, B. CO₂-Expanded Solvents: Unique and Versatile Media for Performing Homogeneous Catalytic Oxidations. J. Am. Chem. Soc. 2002, 124, 2513–2517.
- (14) Kelley, S. P.; Lemert, R. M. Solvatochromic Characterization of the Liquid Phase in Liquid-Supercritical CO₂ Mixtures. AIChE J. 1996, 42, 2047–2056.
- (15) Wyatt, V. T. Characterization of Gas-Expanded Liquids; Georgia Institute of Technology: Atlanta, GA, 2001.

- (16) Zhang, H.; Liu, Z.; Han, B. Critical Points and Phase Behavior of Toluene-CO₂ and Toluene-H₂-CO₂ Mixture in CO₂-Rich Region. J. Supercrit. Fluids **2000**, 18, 185–192.
- (17) Zhang, H.; Han, B.; Li, H.; Hou, Z. Measurement of Critical Points and Phase Behavior of $CH_3OH + CO + CO_2$ Ternary Mixture. J.
- and Phase Benavior of Ch₃OH + CO + CO₂ ferminy bilator. C. Chem. Eng. Data 2001, 46, 130-133.
 (18) Zhang, H.; Han, B.; Hou, Z.; Liu, Z. Measurement of Critical Points of the Methylcyclohexane (MCH)-H₂-CO₂ System in the Distribution of the Methylcyclohexane (MCH)-H₂-CO₂ System CO₂-Rich Region. *Fluid Phase Equilib.* **2001**, *179*, 131–138.
- Gläser, R.; Williardt, J.; Bush, D.; Lazzaroni, M. J.; Eckert, C. A. Application of High-Pressure Phase Equilibria to the Selective (19)Oxidation of Alcohols over Supported Platinum Catalysts in Supercritical Carbon Dioxide. In Utilization of Green House Gases; Liu, C.-j., Mallinson, R. G., Aresta, M., Eds.; ACS Symposium Series; American Chemical Society: Washington, DC, 2003; Vol. 852, pp 352-364.
- (20) Bezanehtak, K.; Combes, G. B.; Dehghani, F.; Foster, N. R.; Tomasko, D. L. Vapor-Liquid Equilibrium for Binary Systems of Carbon Dioxide + Methanol, Hydrogen + Methanol, and Hydrogen + Carbon Dioxide at High Pressures. J. Chem. Eng. Data 2002, 47, 161–168.
- (21) Bezanehtak, K.; Dehghani, F.; Foster, N. R. Vapor-Liquid Equilibrium for the Carbon Dioxide + Hydrogen + Methanol Ternary System. J. Chem. Eng. Data **2004**, 49, 430-434.
- (22) Jessop, P. G.; Stanley, R. R.; Brown, R. A.; Eckert, C. A.; Liotta, C. L.; Ngo, T. T.; Pollet, P. Neoteric Solvents for Asymmetric Hydrogenation: Supercritical Fluids, Ionic Liquids, and Expanded Ionic Liquids. Green Chem. 2003, 5, 123–128. (23) Brown, J. S.; Hallett, J. P.; Bush, D. M.; Eckert, C. A. Liquid–
- Liquid Equilibria for Binary Mixtures of Water + Acetophenone, + 1-Octanol, + Anisole, and + Toluene from 370 K to 550 K. J. Chem. Eng. Data **2000**, 45, 846-850.
- (24) Levitin, G.; Bush, D.; Eckert, C. A.; Hess, D. W. Phase Behavior and Modeling of CO2/Methanol/Tetramethylammonium Bicarbonate and CO2/Methanol/Tetramethylammonium Bicarbonate/ Water Mixtures at High Pressures. J. Chem. Eng. Data 2004, 49.599-606.
- (25) Span, R.; Wagner, W. A New Equation of State for Carbon Dioxide Covering the Fluid Region from the Triple-Point Temperature to

1100 K at Pressures up to 800 MPa. J. Phys. Chem. Ref. Data 1996, 25, 1509-1596.

- (26) BYU. DIPPR 801 Database, 2002.
- (27) Katayama, T.; Ohgaki, K.; Maekawa, G.; Goto, M.; Nagano, T. Isothermal Vapor-Liquid Equilibria of Acetone-Carbon Dioxide and Methanol-Carbon Dioxide Systems at High Pressure. J. Chem. Eng. Jpn. 1975, 8, 89–92. Stryjek, R.; Vera, J. H. An Improved Peng–Robinson Equation of State for Accurate Vapor-Liquid Equilibrium Calculations. Can.
- (28)
- J. Chem. Eng. 1986, 64, 334–340.
 (29) Polishuk, I.; Wisniak, J.; Segura, H. Simultaneous Prediction of the Critical and Sub-Critical Phase Behavior in Mixtures Using Equation of State I. Carbon. Dioxide - Alkanols Chem. Eng. Sci.
- **2001**, *56*, 6485–6510. (30) Huron, M.-J.; Vidal, J. New Mixing Rules in Simple Equations of State for Representing Vapour-Liquid Equilibria of Strongly Non-Ideal Mixtures. Fluid Phase Equilib. 1979, 3, 255-271.
- (31) Renon, H.; Prausnitz, J. M. Local Compositions in Thermodynamic Excess Functions for Liquid Mixtures. AIChE J. 1968, 14, 135 - 144.
- (32) Brunner, E.; Hültenschmidt, W.; Schlichthärle, G. Fluid Mixtures at High Pressure. 4. Isothermal Phase Equilibria in Binary Mixtures Consisting of (Methanol + Hydrogen or Nitrogen or Methane or Carbon Monoxide or Carbon Dioxide). J. Chem. Thermodyn. 1987, 19, 273-291.

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